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IMPROVED STRUCTURAL ADHESIVES FOR BONDING METALS

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BLOOMINGDALE RUBBER COMPANY

DECEMBER 1952

WRIGHT AIR DEVELOPMENT CENTER

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WADC TECHNICAL REPORT 52-156

IMPROVED STRUCTURAL ADHESIVES FOR BONDING METALS

H. C. Engel Bloomingdale Rubber Company

December 1952

Materials Laboratory Contract No. AF 33(038)-21669 RDO No. 604-302

Wright Air Development Center Air Research and Development Command United States Air Force Wright-Patterson Air Force Base, Ohio

FOREWORD

This report describes the work performed by Bloomingdale Rubber Company under Contract No. AF 33(038)-21669, Research and Development Order No. 604-302, "Structural Adhesives", for the period 6 March 1951 to 1 April 1952. The project was administered under the direction of the Structural Design Data Branch, Materials Laboratory, Directorate of Research, Wright Air Development Center, with Major T. J. Martin acting as project engineer.

ABSTRACT

Work under USAF Contract No. AF 33(038)-21669 has been directed toward the development of an improved structural adhesive for bonding metals. An adhesive designated as PA-101, developed and tested under this contract, meets most of the research objectives and so far as is now known conforms to the requirements of Specification 14164. The PA-101 formulation has been evaluated as a two-part, liquid adhesive.

PUBLICATION REVIEW

This report has been reviewed and is approved.

FOR THE COMMANDING GENERAL:

M. E. SORTE

Colonel, USAF

Chief, Materials Laboratory

Directorate of Research

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I. INTRODUCTION

This report is a general summary of the work on Research Contract AF 33(038)-21669 from April 1, 1951 to April 1, 1952. It reviews the experimental work done and discusses formulation, manufacture and properties of the cement developed.

II. RESEARCH OBJECTIVES

Research objectives as contained in Exhibit A of the contract and, as more fully amplified by later conferences between the Contractors' and the Materials Laboratories' representatives, may be summarized as the development of an adhesive having a maximum of the desirable characteristics outlined below:

- (1) Strength and durability characteristics to conform with Specification 14164.
- (2) Required curing temperatures and pressures should allow user relatively wide latitude to facilitate production.
- (3) The adhesive should be capable of production under practical conditions in unlimited quantities, and preferably with readily available commercial equipment. Critical manufacturing variables should be held to a minimum.
- (4) Application characteristics to be superior to those of best commercial present day adhesives. Adhesive should preferably be available as 100% solids or as a film which does not require a companion primer having critical application requirements.
- (5) Metal cleaning methods should be simple and non-critical to facilitate production of reliable bonds.
- (6) The adhesive should be not only non-corrosive on all common metals, including magnesium, aluminum and ferrous alloys, but should as a film afford substantial protection to the metal against corrosion.

In a word, this program was aimed at the development of an adhesive equal to or better than present commercial adhesives, but having sufficient latitude in bonding pressure, bonding temperature, film thickness, and surface cleanliness requirements to simplify manufacturing methods and to aid in the development of consistent bond strength and environmental resistance properties.

III. SUMMARY AND CONCLUSIONS

The adhesive designated in this report as PA-101, developed under Research Contract AF 33(038)-21669, has satisfactorily passed the requirements of this contract as outlined in the objective of this report. It has also satisfactorily met the strength requirements and fluid exposure resistance of U.S.A.F. Specification 14164 for all of the tests performed on bonds cured at 300°F and 250°F. Fatigue strength at standard and low temperature, Bend tests and Impact strength at standard and low temperature are yet to be run.

This cement is a two-part type consisting of Buna N synthetic rubber and phenolic resins compounded with suitable vulcanizing agents and accelerators for satisfactory cures at moderate temperatures of 200°F to 300°F. It may be manufactured by simple milling procedures sufficient for smooth blending of the batch and subsequent solution in methyl ethyl ketone solvent.

The aging characteristics of both part 1 and part 2 of PA-101 cement have been tested up to three months with satisfactory results.

Maximum bond strengths are obtained using 100 psi bonding pressure or higher; however 50 psi produces bonds which pass U.S.A.F. Specification 14164.

Several cleaning methods such as Sprex AC alkaline bath, acetone wipe and chromic-sulfuric acid etch result in bond strengths above 3800 psi at 76°F and above 2100 psi at 180°F for cures at 250°F and 300°F.

IV. EXPERIMENTAL METHODS

All test samples were prepared using .06 μ inch 2μ S-T 3 Alclad metal bonded at $1/2^m$ depth of lap.

The metal was cleaned by first removing the excess oil and dirt by wiping with acetone. It was then immersed in a chromic-sulfuric acid solution for ten minutes at 160°F. The acid solution was composed of the following:

chromic acid flake

5 oz./gal.

Conc. sulfuric acid (technical) 23 oz./gal.

The metal was rinsed thoroughly in hot running water and dried in an oven.

Although other cleaning methods were tested in separate experiments, the above method was followed throughout the contract for all formula evaluations. Two brush coats of adhesive were applied to the metal within eight hours of the cleaning operation. The adhesive was air dried for sixteen hours followed by an oven dry of one hour at 150°F. The test panels were assembled and cured in an electrically heated platin press at a bonding pressure of 100 psi according to the following temperature—time schedule:

Temperature	Time in
· op	Minutes .
300	20
275	30
250	45
225	70
200	90

The cured glue line thickness was controlled at $0.003^{\circ} \pm 0.0005^{\circ}$ except where deliberately varied for test purposes.

Cured test panels were cut into one inch wide coupons numbered consecutively across the panel. All tests were conducted on a Dillon Testing Machine using a loading rate of 600 to 700 psi per minute. Tests at 180°F were conducted by enclosing the upper part of the testing machine in an insulated and heated cabinet. A similar cabinet packed with dry ice was used for tests at -70°F. All temperatures were measured by means of a thermo-couple clamped to the

specimen at the glue line. The ultimate load was determined to the nearest 5 pound increment. The length and width of each bond area was measured to the nearest 0.01 inch and the shear stress in the adhesive calculated in pounds per square inch for each test coupon.

V. DISCUSSION

The first experimental studies were conducted on formulations based on poly acrylic rubber-phenolic resin blends. Forty-six formulations consisting of Hycar PA-21 and various commercial phenolic resins with several vulcanizing systems were tested. Although several cements were developed of this general type which gave bond strengths over 2500 psi when cured at 200°F and over 3000 psi when cured at 300°F, the strength at -70°F was uniformly poor (below 800 psi) due to the embrittlement of the poly acrylic rubber constituent. Therefore this line of investigation was shifted to nitrile rubber-phenolic resin formulations.

Of the nitrile rubber types available Hycar OR-25ST was selected because of its ready solubility in common solvents, simple milling procedure requirements, good solution stability, and satisfactory strength properties over a wide temperature range. The formulation studies conducted were aimed at (a) selection of satisfactory phenolic resins, (b) development of a vulcanization system capable of curing below the 325°F temperature normally used, (c) reasonable stability of solutions containing so reactive a system, (d) satisfactory filler reinforcement.

A total of sixty-two cement formulations based on nitrile rubber Hycar CR-25ST were studied. Since the vulcanization system required for curing at 200°F and 250°F was also reactive at normal temperatures and therefore affected solution stability a two-part cement formulation was necessary. The more reactive phenolic resins satisfactory for curing at low temperatures with the nitrile rubber were also found to be mutually reactive in the same solution and hence resulted in lowered bond strength after solution aging of the rubber and phenolic resins together. Since bond strength at -70°F of the nitrile rubber cements studied were uniformly high, no formulation modification was necessary in order to meet this requirement. Therefore the nitrile rubber and phenolic resins were kept in separate parts and each of the remaining constituents such as carbon black filler, zinc oxide, stearic acid, sulfur, Agerite Resin D, Captax and Butyl Eight were tested for stability after aging with either the rubber or the phenolic resins. Satisfactory solution stability in methyl ethyl ketone was obtained by milling the rubber sufficiently to blend the carbon filler, the stearic acid, zinc oxide and Agerite Resin D. However, it was found that the accelerator Butyl Eight was not stable when mixed with the phenolic resin as Part 2 of the cement, but remained stable in the rubber solution provided no sulfur or Captax were present. The sulfur and Captax were finely ground and dispersed thoroughly in the powdered phenolic resins. This latter mixture, stable in dry powder form, is then added to the rubber solution at the time of use. This cement, designated PA-101, is prepared as follows:

	•	PART 1		• •
٦.	Constituent Hycar OR-25ST		Parts by weig	tht Band on cold rolls.
	ny car on-zyor		1.00	pand on cold lotte.
2.	Pilletex Carbon black SRF		50	Add to rubber and
•	64		_	mill 16 minutes.
3•	Stearic acid		1	Add items 3, 4 and
4.	Zinc Oxide		5	5 and mill for 5 minutes.
MAD	אל מיים דה זול	•	•	•
WAD	C TR 52-156	3		

PART 1 (Conv'd)

5.	Constituent Agerite Resin D	Parts by weight	Dissolve in methyl ethyl ketone at 20% solids.
6.	Butyl Eight	7	Add to above solution.
		PART 2	
1.	Bakelite 18773	50	Grind items 3 and 4 and thoroughly disperse
2.	Durez 7031 A	50	with items 1 and 2 to form
3•	Captax	2	homogeneous dry powder.
4.	Sulfur	3	Sift

At the time of use 12.8g of Part 2 powder are added to 100g of Part 1 solution and stirred thoroughly for three to five minutes.

Tables 1 and 2 present the test data on PA-101 cured at 300°F and 250°F respectively and tested against the requirements of U.S.A.F. Specification 14164. The tests performed consisted of dry shear strength at 76°, 180°F and -70°F, shear strength at 76°F after 7 days immersion in isopropyl alcohol, ethylene glycol, hydraulic oil, hydrocarbon fluid and after 30 days immersion in water. Part of these data were previously presented in Report No. 11 but are repeated here in order to present the complete data obtained for this specification in the final report.

Samples for fatigue testing at 76°F and -70°F were prepared and forwarded to the Materials Laboratory, Wright air Development Center.

Table 3 presents test data on samples prepared from metal cleaned by the follow⊷ ing methods: (a) immersion in a Sprex AC alkaline solution for 10 minutes at 160°F; (b) wipe with clean cloth wet with acetone; (c) wash with soap and water; (d) immersion in Sprex AC alkaline solution followed by an acid etch in a chromicsulfuric acid solution, 10 minutes at 160°F. Cleaning by wiping with acetone gave bond strengths of 3950 psi and 3850 psi at 76°F and 2175 psi and 2000 psi at 180°F for 300°F and 250°F cures respectively. These shear strengths compare very favorably with those obtained using chemical cleaning methods such as Sprex AC alkaline solution which gave 3945 psi and 4375 psi at 760F, and 2250 psi and 2150 psi at 180°F. Sprex AC alkaline cleaner followed by a chromic-sulfuric acid etch resulted in bond strengths of 4000 psi and 4100 psi at 76°F and 2350 psi and 2115 psi at 180°F. Cleaning by scap and water resulted in definitely inferior adhesion. During the progress of the test program it was found that one variable which influenced the shear strength of the rubber based adhesives was the thickness of the glue line; therefore this factor was controlled at .003 inch ± .001 inch in as much as possible on all test samples prepared using PA-65 cement and all subsequent formulas. A series of test panels was then prepared using PA-101 cement in which an attempt was made to obtain cured glue lines varying from .002 to .008 inch. Samples were made using from one to six brush coats of adhesive on each faying surface. However the heavier applications of adhesive did not result in thicker cured glue lines. This was due in all probability to the

increased flow (at equal pressure) of the thicker films. Examination of the data shows that the shear strength varies as a function of the number of coats of administration applied rather than in direct proportion to the cured glue line thickness. This may possibly be explained by greater solvent retention of the thicker film. Table h lists the detailed test data.

Table 5 gives the test data obtained from panels bended at 50 psi as compared with two samples bonded at 100 psi. The lower bonding pressure caused a loss of 22 per cent in shear strength at 76°F and 16 per cent at 180°F.

Table 6 lists the average shear strength data on all adhesive formulas as developed on this contract for 300°F and 200°F or 250°F cures when tested at 76°F and 180°F. These formulas PA-45 through PA-108 were of the Buna N-Phenolic Resintype.

Tables 7 through 17 present all formulations studied during the contract and Table 18 lists and briefly describes all materials used in the various formulations.

Cement formulas PA-1 through PA-18, PA-22, 23, 24, 29, 33, 35 and 36 consisted of preliminary studies of simple blends of Hycar-PA 21 poly acrylic synthetic rubber with various phenolic resins for qualitative evaluation only therefore these materials are not listed in the tables of cement formulas. Duplicate formulations occasionally appear, in some cases variations in milling procedures were used. The detailed variation used is described in the monthly reports. In other instances two-part cements were prepared with different placement of the ingredients in order to obtain optimum stability of the two parts.

All of the adhesives were prepared using methyl ethyl ketone solvent except as noted below. The solids content of the cements as mixed for application was 29.1 per cent. In PA-97 adhesive a solvent blend was used consisting of ethylene dichloride 40 parts, methyl ethyl ketone 40 parts and denatured alcohol 20 parts by weight.

In PA-80 and PA-81 a solvent blend was used consisting of ethylene dichloride 40 parts, toluene 40 parts, methyl ethyl ketone 6 parts, secondary butyl alcohol 18 parts and denatured alcohol 18 parts by weight.

Table 1
TEST DATA OBTAINED ON PA-101 CEMENT

CURED AT 300°F

Sample No.	Test	Specification Requirement psi		Shear strength of PA-101, psi
766 -1 -5 -1 0	Shear at 76 ⁰ F	2500 min.		4200 4400 4250
76 7-1				4350
 5				4550
-10				<u>4200</u>
			AV =	4325
766-2	Shear at,	1250 min.		2450
767 – 2	180 ⁰ f			<u> 2550</u>
			AV =	2500
766-3	Shear at	2500 min.		5050
767-3	-70° F	•		5450
			AV =	5250
774-1	Shear at	2000 AV.		3890(Control-not
-2	76 ⁰ F after			4100 immersed)
-3	7 days			4150
74567 6	immersion			4150
~5 6	in isopropyl			4200
= €	alcohol (AN-F-13)			4100 4200
_G	(WII-LATO)			4300
- 9				4000
-10				4000
-11				3950
			AV =	4114
776-1	Shear at	2000 AV.		5990(Control-not
-2	76°F after			4050 immersed)
-3	7 days			4200
-4	immersion in			4350
-5	ethylene			4250
 6	glycol (AN-E-2)			4250
-5 -6 -7 -9	(Alv-L-C)			4255
 C				4240
3 70				4210
-10 -11				3900 3800
			A Titor	\ <u></u>
	•		AV ≈	4151

Table 1 Continued - TEST DATA OBTAINED ON PA-101 CEMENT CURED AT 300°F

778-1 -2 -3 -4 -5 -6 -7 -8 -9 -10 -11	Shear at 76°F after 7 days immersion in hydraulic oil (AN-0-366)	2000 Av.	AV. =	4182 4050 4150 4100 4300 4350 4200 4200 4210 4200 4100
780-1 -2 -3 -4 -5 -6 -7 -8 -9 -10 -11	Shear at 76°F after 7 days immersion in hydrocarbon fluid	2000 AV.	AV. =	3825(control -not 4315 immersed) 4365 4365 4365 4215 4315 4460 4170 4115 3970
772-1 -2 -3 -4 -5 -6 -7 -6 -9 -10 -11	Shear at 76°F after 30 days immersion in water	2000 AV.	AV. =	4060 3645 4220 4270 4220 5335 4270 4215 4165 5855 3490
776-4	Long time strength at 180°F	800 psi		315 hours no failure

Table 2
TEST DATA OBTAINED ON PA-101 CEMENT

CURED AT 2500

Sample No.	Test	Specification Requirement psi		Shear Strength of PA-101. psi
768-1 -5 -10 769-1 -5 -10	Sheat at 76 ⁰ F	2500 min.		4100 4400 4000 4300 4500 4400
			AV. =	4300
768 -2 769 - 2	Shear at 180°F	1250 min.		1950 <u>1955</u>
			AV. =	1952
768 –3 769 –3	Shear at -70°F	2500 min.		4850 5100
			AV. =	4975
775-1 -2 -3 -4 -5 -6 -7 -8 -9 -10 -11	Shear at 76°F after 7 days immersion in isopropyl alcohol (AN-F-13)	2000 Av.	AV. =	4130(control -not) 4110 immersed) 4190 4200 4250 4200 4205 4200 4050 4050 3800
777-1 -2 -3 -4 -5 -6 -7 -8 -9 -10 -11	Shear at 76° after 7 days immersion in ethylene glycol (AN-E-2)	2000 AV.	AV. =	4130 4500(control -not 4410 immersed) 4360 4365 4355 4260 4360 4510 4360 4215 3625 4282

Table 2 Continued - TEST DATA OBTAINED ON PA-101 CEMENT CURED AT 250°F

779-1 -2 -3 -4 -5 -6 -7 -8 -9 -10 -11	Shear at 76°F after 7 days immersion in hydraulic oil (AN-0-366)	2000 AV.		4185(Control-not 4450 immersed) 4455 4550 4650 4600 4610 4450 4450 4445
			AV. =	4501
781-1 -2 -3 -4 -5 -6 -7 -8 -9 -10 -11	Shear at 76°F after 7 days immersion in hydro-carbon fluid	2000 AV.	AV. =	3200(Control-not 4600 immersed) 4550 4450 4350 4350 4400 4500 4500 4450 3050
773_1 _2 _3 _4 _5 _6 _7 _9 _10 _11	Shear at 76°F after 30 days immersion in water	2000 AV.	AV. =	4250(control-not 4050 immersed) 4350 4600 4500 4600 4700 4950 4850 4700 4050

Table 5

BFFECT OF SURFACE PREPARATION OF ALUMINUM
ON BOND STRENGTH PA-101 ADHRSIVE

Sample No.	Curing Temperature o _F	Cleaning Method	Shear in Adhesive psi at 76°F	Shear in Adhesive psi at 180°F
905-1	300	Sprex AC	4020	
-2		alkaline	3870	
-3		bath, 10		2250
-4		minutes at		2250
-5		160°F		2250
906-1	250	Sprex AC	4350	
-2		alkaline	4400	
~ 5		bath, 10		2050
-4		minutes at		2150
-5		160°F		2250
907-1	300	Acetone	3 900	
-2		Wipe	4000	
-2 -3 -4				2200
- -5				2150
-5 908-1	250	Acetone	3675	2150
_5 2∩0⊶7	230	Wipe	4030	
		urbe	4000	1990
=				2040
* ? 1 5				1940
909-1	300	Soap	3550	2010
-2		and	3850	
-3		Water		2000
-4			•	2050
- 5				2000
910-1	250	Soap	2950	
-2		and	300 0	
-5		Water		1600
4		•		1350
- 5	500			1200
920-1	300	Sprex AC	3950	•
- -2 3		and	4050	• • • •
4		chromic-		2400
 5		sulfuric acid		2550
918-1	250	Sprex AC	4900	2500
-2	~~~	and	4200 4000	
- 5		chromic-	2000	2100
-4		sulfuric		2150
-5		acid		2100
•				~ TOO

Table 4

INFLUENCE OF NUMBER OF APPLICATION COATS
ON STRENGTH PROPERTIES OF PA-101 CEMENT

Sample No.	Number of Coats	Cured Thickness in in.	Shear in Adhesive psi at 76°F	Shear in Adhesive psi at 130°F
930-1	One	•0025	3580	
-2		W	3530	1960
-3	300°	₩ •		2060
4 - 5	Cure	•		2060
931-1	One	.002	34 80	
-2	0.500	*	3630	1 <i>ee</i> E
-3	250°	N		1665 1765
-4 - 5	Cure	•0025		1860
917-1	Two	•003	3900	
91/ - 1	140	*	5700	
-3	300°	•	0.00	2100
-4	Cure	*		2200
~ 5	•	*		2150
918-1	Two	•003	4200 4000	
- ર - ઠ	250°		4000	2100
-4	Cure	•		2150
- 5	5 5	•		2100
922 -1 -2	Three	•0055	4000 3970	
-3	300°	*	0310	1960
-4	Cure	•005		2155
-5	040	•0045		2115
923-1	Three	•006 •0055	4350 4350	
جد ح3	250°	•0055 •005	#00U	1900
-4	Cure	N		2000
- 5	,	•		1850
924 -1	Four	.006 .0055	5920 5970	
	300°	•0045	0310	1865
<u>~</u>	Cure	•00£5 •005		1910
લુસ ન ન		*		1960

Table 4 Continued - INFLUENCE OF NUMBER OF APPLICATION COATS ON STRENGTH PROPERTIES OF PA-101 CEMENT

Sample No.	Number of Coats	Cured Thickness in in.	Shear in Adhesive psi at 76°F	Shear in Adhesive psi at 180°F
925-1	Four	•0065	3870	
-2		•0055	3970	
~3	250°	•0045	0370	1325
-4	Cure	•005		1470
-5		.0045		1375
926-1	Five	•0065	3725	
		•006	3775	
-2 -3	300°	•005	0110	1420
-4	Cure	*		1600
- 5		•		1600
927-1	Five	•005	367 5	
-2		•0055	3630	
⊸ 3	250 ⁰	•0045		1275
* * * * *	Cure	•0045		1175
~ 5		•005		1175
928-1	Six	•0055	335 9	
-2	6	•005	333 5	
-3	500 ⁶	•0045		1080
-4	Cure	N		1130
- 5		•		1030
929-1	Six	•005	3300	
-2	O	•005	3350	
-3	250 ⁰	•0045		950
-4	Cure	•004		1050
≈ 5		•004		1000

Table 5
INFLUENCE OF BONDING PRESSURE ON SHEAR STRENGTH OF PA-101 CEMENT

Sample No.	Curing Temperature o _F	Pressure psi	Shear in Adhesive psi at 76°F	Shear in Adhesive psi at 180°F
903-1	300	50	3250 3350	
 2 3 4 5			3330	1815 1855 1915
904-1 -2 -3 -4 -5	250	50	3000 3250	1550 1500 1400
827 - 1 -2 -3 -4 -5	300	100	4000 4000	2100 2150 2000
828-1 -2 -3 -4 -5	250	100	4200 4200	1900 1900 1850

AVERAGE SHEAR STRENGTH TEST DATA ON ALL ADHRSIVE FORMULATIONS
OF BUNA N- PHENOLIC RESIN TYPE

Adhesive Designation	Curing Temperature ^o F	Average Shear -70°F	Strength psi at: +76°F +180°F	
PA-45	300	4195	1560	
PA-46	300	4755	2960	
PA-46	250	4367	2500	
PA-46	200	3170	2140	
PA-47				
PA-48	300		3 060 7 75	
PA-49	500		3620 160	
PA-49	200		2510 190	
PA-50	500	4000	3550 475	
PA-50	200		2520 197	
PA-51	300	3990	2550 1170	
PA-52	300		3600 1065	
PA-54	500		2710 1000	
PA-54	200		2050 47	
PA-55	200		3405 100	
PA-56	200		3320 65	
PA-57	200		3210 1070	
PA-58	200		2100 550	
PA-59	200		1275 315	
PA-60	200		2211 222	
PA-61	200		1420 570	
PA-62	200		1455 720	
PA-63	200		925 165	

AVERAGE SHEAR STRENGTH TEST DATA ON ALL ADHESIVE FORMULATIONS
OF BUNA N- PHENOLIC RESIN TYPE

Adhesive Designation	Curing Temperature ^O F	Average Spear -70°F	Strength psi	at: +180°F
PA-G4	200		1225	195
PA-G5	200		2800	1350
PA-66	200		2170	665
PA-67	200		2650	930
PA-67	200		850	390
PA-67	300		3820	2700
PA-67	300		3200	1350
PA-68			Very poor	
PA-69	300		34 50	2400
PA-69	200		2070	1250
PA-70	30C	,	3620	2745
PA-70	200		2950	1175
PA-71	200		2480	740
PA-72	200		2730	970
PA-74	200		1760	505
PA-74	300		2700	1820
PA~75	200		2450	62 5
PA-75	300		3600	2300
PA-76	200		3270	1870
PA-76	300		3200	1870
PA-77	200		1520	430
PA-77	300		3550	2020

Table 6 (con't)

AVERACE SHEAR STRENGTH TEST DATA ON ALL ADHESIVE FORMULATIONS
OF BUNA N- PHENOLIC RESIN TYPE

Adhesive Designation	Curing Temperature ^O F	Average Shear -70°F	Strength 476°F	psi at: +180°F
PA-78			Very poor	•
PA-79	200		2450	670
PA-79	300		1905	1060
PA-80	200		2450	745
PA-80	300		3925	2700
PA-81	200		690	180
PA-81	300		1650	710
PA-62	300		2400	1405
PA-82	200		2400	425
PA-83	300		2830	1720
PA-83	200		3300	525
PA-84	300	•	2030	570
PA-84	200		585	250
PA25	300		2900	1700
PA-65	200		2870	610
PA-86	Very poor			
PA-87	300		2770	1980
PA-87	200		2220	560
PA-88	300		3440	2180
PA-68	200		2130	690
PA=89	300		3170	1720
PA89	200		1625	480

Table 6 (con't)

AVERAGE SHEAR STRENGTH TEST DATA ON ALL ADHESIVE FORMULATIONS

OF BUNA N- PHENOLIC RESIN TYPE

Adhesive Designation	Curing Temperature ^O F	Average Shear -70°F	Strength 476°F	psi at: \$180°F
PA-90	300		2630	1920
PA-90	200		2340	175
PA-91	300		2275	850
PA-91	200		1200	255
PA-92	300		1500	440
PA-92	200		Failed in	machining
PA-95	300		3720	1700
PA-93	200		1200	3 05
PA-94	300		3160	1610
PA-94	200		1515	445
PA-95	300		3000	2460
PA-95	200		1410	395
PA- 96	300		1850	715
PA-9 6	200		680	92
PA-97	300		2370	970
PA-97	200		500	200
PA-98	300		3430	1480
PA-98	200		2460	480
PA-99	500		377 5	1820
PA-9 9	200		5106	700
PA-100	500		3640	2060
PA-100	200		2800	870

Table 6 (Con't)

AVERAGE SHEAR STRENGTH TEST DATA ON ALL ADHESIVE FORMULATIONS
OF BUNA N- PHENOLIC RESIN TYPE

Adhesive Designation	Curing Temperature F	Average Shear -70°F	Strength 476 F	psi at: +180°F
PA-101	50 0	5250	4325	2500
PA-101	200		3500	1050
PA-101	250	4975	4230	2010
PA-102	300		2590	1555
PA-102	250		2200	740
PA-103	300		3805	2200
PA-103	250		5825	1830
PA-104	300		5975	1960
PA-104	250		5200	1420
PA-105	300		3815	2120
PA-105	250		4010	1370
PA-106	300		3725	1380
PA-106	250		2775	900
PA-107	500		3975	2390
PA-107	250		4050	2240
PA-108	500		3825	
PA-108	250		3875	1860 1545
			0019	T9#9

WADC TR 52-156

Formula

19

PA-7 22 ADHESIVE FORMULATIONS - PA-1 THROUGH PA-10 PA-6 20 PA-5 ည PA-4 20 හු PA-3 ည 20 PA-1 PA-2 ည 20

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Hycar PA-21

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Bakelite BR 5360

Durez 12687

Durez 590

PA-10

PA-9

PA-8

Table 7

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ည 20 က္သ Bakelite RD-4953 Synvar RC 50 D Durez 7031-A

Vinyl chloride acetate Epon 1007

Elvaset 41 A 95

Vinyl acetate AYAF

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aT.	3

ADHESIVE FORMULATIONS - PA-11 THROUGH PA-18

TR 52-	Formula No.	PA-11	PA-12	PA-13	PA-14	PA-15	PA-16	PA-17	PA-13
156	Hycar PA-21	20	20	20	20	20	50	50	50
	Durez 10390	20							
	Synvar RC 50 D plus 10% hexa		20						
	Durez 175			20					
	Durez 14574		÷		20				
	Durez 11078					20			
20	Marbon 8000						20		
	Bakelite BR 15401							50	
	Durez 10305								50

WADC

Table 9

•			ADHESI	ADHESIVE FORMULATIONS - PA-19 through PA-54	ULATION	S - PA-	19 thro	ugh PA-	24		
Formuls No.	PA-19	PA-19 PA-20 PA-21 PA-25 PA-26	PA-21	PA-25	PA-26	PA-27	PA-28	PA-30	PA31	PA-27 PA-28 PA-50 PA-51 PA-52 PA-54	PA34
Hycar PA-21	100	700	100	100	100	100	100	100	100	100	100
SRF Carbon Black	20	20	20	82	20	20	20	20	20	20	20
Sulfur	4	4	4	œ	œ	©	4	4	ず	4	4
Trimene Base	4	4	4	せ	4	4			4		4
Durez 12687	100			100			001	r			
Ourez 7031-å		001			100						
Bakelite RD-49-33	53		700			001					
Bakelite 18791								700	100		
Bakelite 18773										300	
Bakelite 50-63											001

ADHESIVE FORMULATIONS - PA-37 through PA-47

Table 11

	-	NITRILE	RUBBER	PA-18	NITRILE RUBBER-PHENOLIC RESIN ADHESIVE FORMULATIONS PA-48 THROUGH PA-55	IN ADE	ESIVE	FORMUI	ATIONS	_
	•					,		:		
Formula No.	48	484	48B	49	20	51	52	23	22,	25
Hy car OR25ST	700	100	97	100	900	700	100	700	9	100
Carbon Black SRF	20	20	20	20	20	20	75	20	20	75
Zinc Oxide				ည	က				ડ	
Sulfur	7	4	4		0.5	4	4	4	4	4
Stearic Acid										
Diatoma ceous Earth				હ્ય	લ				Q	
Bakelite RD-49-33	20	20	75	75	75	20	20	20		20
Durez 12687	20	20	75	75	75	20	20	20		20
Captax		н		Н	н					
Tuads				10	æ					
Agerite Resin D				α	લ				લ	
Silene EF						ខ្ព				
Durez 7031-A									150	

NITRILE RUBBER-PHENOLIC RESIN ADHESIVE FORMULATIONS PA-56 THROUGH PA-66

Formula No.	56	57	28	29	8	61	88	83	2	65	99
Hycar OR25 ST	100	200	100	ğ	8	8	8	801	ğ	82	82
Carbon Black SRF	20	20	20	20	20	20	20	20	20	20	20
Zinc Oxide		Ŋ	ល	ស	ស	ស	ហ	ហ	ល	ហ	ល
Sulfur	æ	10	10	ю	ю	ю	ю	જ	ю	ю	ю
Stearic Acid		Н	H	H	Н	н	7	Н	ч	러	н
Diatemaceous Earth											
Bakelite ND-49-53	20	20	20	20	20	20	45	50	20	20	20
Dures. 12687	20	20	20	20	20	8	45	20	20	20	20
Captax		લ	R	લ	н	Н	Q	-	-	Q	Q
TUADS											
Agerite Resin D		~	н	-	H	Н	7	Н	٦	н	
Butyl Bight		7				7	2	7		7	7
Hexamethylenetetramine				ស							
Methyl Zimate					਼ ਼	다.		1.1	1.1		
Bakelite BR-7							ω				
Paraformaldehyde							Q				
Butyl Zimate											1.1

Table 13

NITRILE RUBBER - PHENOLIC RESIN ADHESIVE FORMULATIONS
PA -67 THROUGH PA-75

Formula No.	PA-67	PA-68 PA-69	PA-69	PA-70	PA-71 PA-72		PAST 3	DAMA	P.A. or 87 5
Hycar OR-255T	100	100	100	100	700	100	200	100	300
Carbon Black SRF	50	20	20	20	20	20	ಜ		22
Carbon Black HMF								S	
Sulfur	29	ю	80	က	ю	ю	ૹ	ಣ	6 73
Stearic Acid	ч	н	н	н	н	н	5 7-1	કર્સ્ય	gund.
Zinc Oxide	വ	ល	ស	വ	ഹ	ល	ĽĴ	មា	េ
Agerite Resin D	ч	н	rł	H	I	ч	galanter .	- ground	p~4
Captax	ત્ય	લ્ય	લ	હ	ત્ય	લ		હ્ય	લ્ય
Butyl Eight	7	7	2	7	7	7	Fig. 20	C	£
Durez 7031-A	20	20	20	20	75	150		S	S
Bakelite 18773	20	20	20	20	75		ũ	ß	Ĉ
Durez 12687									
Nitropropane		700							
Boron Fluoride Phenol Complex BF ₃ Parlon 125 cps				ત્ય					

Table 14

NITRILE RUBBER - PHENOLIC RESIN ADHESIVE FORMULATIONS
PA-76 THROUGH PA-65

	Formula No.	PA-76	PA-77	PA-78	PA-79	PA-80	PA01	PA82	PA82 PA03 PA04	PA-84	PA-85
	Hycar CR-25ST	100	100	700	100	100	100	100	100	100	90
	Carbon Black SRF	20	20	20	20	20	20	20	20	22	20
	Sulfur	ю	ю	ю	ĸ	ю	10	က	ю	ю	ю
	Stearic Acid	н	н	H	-	н	H	H	ч	ч	н
	Zinc Oxide	ស	ស	ហ	ശ	ស	ស	rv	ស	ιΩ	ស
	Agerite Resin D	н	н	н	ч	н	н	н	т	Н	H
	Captax	es.	œ	Q	લ	લ	æ	લ	es.	શ	œ
	Butyl Eight	7	2		7	7	7	7	4	2	7
	Durez 7051-A	20	20	20	20	22	20	20	20		100
	Bakelite 18773	20	50	20	22	20	20	20	20	100	
	Mica	20									
	Litharge			લ							
,	Boron Fluoride Ammonia Complex				N						

Chemigum N3NS

Table 15

NITRILE RUBBER - PHENOLIC RESIN ADHESIVE FORMULATIONS
PA-36 THROUGH PA-94

Formula No.	PA-86	PA67 PA68	- (PA-89	PA-90	PA-91	PA-92	PA-93	PA-94
Hycar OR-25ST	100	100	100	100	001	100	100	100	100
Carbon Black SRF	20		20	20	20	20		20	
Sulfur	အ	ເດ	co ₄	ю	ю	ю	яĢ	ю	ะง
Stearic Acid	н	н	Н	н	rel	н	ч	н	ч
Zinc Oxide	ស	ស	ហ	ស	ស	ល	ស	ហ	ro
Agerite Resin D	н	н	~	н	н	Ħ	rH	٦	Ħ
Captax	cv.	ત્ય	€ લ	€ .	€	લ	∾	€	જ
Butyl Eight	7	7	2	4	7	7	7	7	7
Varcum 5138	100								
Carbon Black EPC		20							
Durez 7051-4		100	20				20		20
Durez 12687			20						
Durez 10128 plus hexa				20	100	53.7		%	
Bakelite 18773				50		46.3	20	20	20
Alcoa Powder R-20							20		
Iron Oxide No. 507									20

Table 16

NITRILE RUBBER - PHENOLIC RESIN ADHESIVE FORMULATIONS
PA-95 THROUGH PA-100

			4	*	XX	
Formula No.	PA-95	PA-96	PA-95 PA-96 PA-97 PA-98	PA-98	PA=99	Part 1 Part 2
Hycar OR-25ST			100	100	100	100
Hycar OR-15EP	100	100				
Carbon Black SRF	20	20	20	20	20	50
Sulfur	ŧ0	60	ю	ĸ	ю	80
Stearic Acid	н	H	н	7	н	rł
Zinc Oxide	ស	ស	ro	ນ	വ	ശ
Agerite Resin D	r٠	н	н	н	H	rt
Captax	હ	œ	œ	€2	લ્ય	જ
Butyl Bight	7	7	7	7	7	4
Durez 7031-4	20	20	20	20		20
Bakelite 18773	20	20	20			50
.Bakelite 18775 Partially cured				20	20	
Durez 7031-A Partially cured					20	

	NITRI	e Rubber	NITRILE RUBBER - PHENOLIC RESIN ADHESIVE FORMULATIONS PA-101 THROUGH PA-108	PHENOLIC RESIN ADHESI PA-101 THROUGH PA-108	VE FORMULA	TIONS	
Formula No.	PA-101 Part 1 & 2	PA-102 Part 1 & 2	PA-104 Part & 2	PA-105 Part	PA-106 Part	PA-107 Part A 2	PA-10
Hycar OR 255T	100	100	100	100	100	100	001
Carbon Black SRF	20	20	20	20	20	20	20
Sulfur	ເນ	1 3	ဗ	60	ю	8 0	
Stearic Acid	H		٦	rt	Н	н	н
Zinc Oxide	2	വ	വ	ស	ស	ហ	ស
Agerite Resin D	н	FI	വ	rt	н	н	ч
Captax	જ	€ €	હ	જ	6	Ø	
Butyl Eight	7		2	7			4

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Bakelite 18773

Durez 7031 A

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Table 18

INDEX TO MATERIALS USED IN ADHESIVE FORMULATIONS

Material Designation	Type	Manufacturer
Agerite Resin D	Rubber antioxidant	Vanderbilt Co., Inc. 230 Park Ave. New York 17, N.Y.
Alcoa Powder R-20	Aluminum oxide filler	The Aluminum Company of America Chemicals Div. Pittsburgh, Penna.
Bakelite RD-49-33	Thermosetting phenolic resin	Bakelite Corp. 30 East 42nd St. New York 17, N.Y.
Bakelite 18791	Thermosetting phenolic resin	Bakelite Corp. 30 East 42nd St. New York 17, N.Y.
Bakelite 18773	Thermosetting phenolic resin	Bakelite Corp. 30 East 42nd St. New York 17, N.Y.
Bakelite 50-63	Thermosetting phenolic resin	Bakelite Corp. 30 East 42nd St. New York 17, N.Y.
Bakelite 18306	Thermosetting phenolic resin	Bakelite Corp. 30 East 42nd St. New York 17, New York
Bakelite 18661	Thermosetting phenolic resin	Bakelite Corp. 30 East 42nd St. New York 17, New York
Bakelite BR-7 Bakelite 3360	Resorcinol resin thermoplastic resin	Bakelite Corp. 30 East 42nd St. New York 17, New York
Boron Fluoride Phenol Complex BF3	Catalyst	Allied Chemical & Dye Corp. General Chemical Division Claymont Development Lab. Marcus Hook, Penna.
Boron Fluoride Ammonia Complex	Catalyst	Allied Chemical & Dye Corp. General Chemical Division Claymont Development Lab. Marcus Hook, Penna.

Table 18 (con't)

INDEX TO MATERIALS USED IN ADHESIVE FORMULATIONS

Material Designation	Туре	Manufacturer
Butyl Eight	Rubber accelerator	Vanderbilt Co. Inc. 230 Park Ave. New York 17, N.Y.
Butyl Zimate	Accelerator for vulcanizing rubber	Vanderbilt Co. Inc. 230 Park Ave. New York 17, N.Y.
Carbon Black SRF	Rubber reinforcer-filler	Binney & Smith Co. P.O. Box 431 Raston, Penna.
Carbon Black EPC	Rubber reinforcer-filler	Binney & Smith Co. P. O. Box 431 Easton, Penna.
Carbon Black HMF	Rubber reinforcer-filler	Binney & Smith Co. P.O. Box 431 Easton, Penna.
Captax	Rubber Accelerator curing agent	Vanderbilt Co., Inc. 230 Park Ave. New York 17, N.Y.
Chemigum N3NS	Nitrile type synthetic rubber	Goodyear Tire & Rubber Co Chemical Division Akron 16, Ohio
Durez 12687	Thermosetting phenolic resin	Durez Plastics and Chemic Corp Walck Road North Tonawanda, N.Y.
Durez 7031-A	Thermosetting phenolic resin	Durez Plastics and Chemic Corp Walck Road North Tonawanda, N.Y.
Durez 10128	Thermosetting phenolic resin	Durez Plastics and Chemic Corp Walck Road North Tonawanda, N.Y.
Durez 590	Thermoplastic resin	Durez Plastics and Chemic
Diatomacious Earth	Filler	Johns-Manville 22 East 40th St. New York 16, N.Y.
Epon 1007	Epoxy type resin	Shell Chemical Corp. 500 Fifth Ave. New York 18, N.Y.
lycar OR-15-EP	Nitrile type synthetic rubber	B. F. Goodrich Chemical Co Rose Building Cleveland 15, Ohio
VADC TR 52-156	31	OTG AGIGIM ID OHIO

Table 18 (con't.)

INDEX TO MATERIALS USED IN ADHESIVE FORMULATIONS

Material Designation	Туре	Manufacturer
Hycar OR-25ST	Nitrile type synthetic rubber	B. F. Goodrich Chemical Co. Rose Building Cleveland 15, Ohio
Hycar PA-21	Polyacrylic type synthetic rubber	B. F. Goodrich Chemical Co. Rose Building Cleveland 15, Ohio
Hexamethylene titramine	Curing agent for phenolic resins	E. I. Du Pont De Nemours & Co., Inc. Wilmington 98, Delaware
Iron Oxide No. 507	Filler	Chas. A. Wagner Co. 813 Callowhill St. Philadelphia 23, Penna.
Litharge	Wilcanizing agent for rubber	E. I. Du Pont De Nemours & Co., Inc. Wilmington 98, Delaware
Methyl Zimate	Accelerator for vulcanizing rubber	Vanderbilt Co., Inc. 230 Park Ave. New York 17, N.Y.
Nica	Filler	The Micalith Corp. York, Penna.
Nitropropane	Anti-gilling agent	Commercial Solvents Corp. 17 East 42nd St. New York 17, New York
Paraformal dehyde	Curing agent	E. I. Du Pont De Nemours & Co., Inc. Wilmington 98, Delaware
Parlon 125 cps	Rubber derivative resin	Hercules Powder Co. Wilmington, Delaware
Silene EF	Filler	Pittsburgh Plate Glass Co. Columbia Chemicals Div. Fifth Ave. & Bellefield Pittsburgh 13, Penna.
Stearic Acid	Activator for zinc oxide in curing rubber	W. C. Hardesty Co. 41 East 42nd St. New York 17, New York

Table 18 (con't.)

INDEX TO MATERIALS USED IN ADHESIVE FORMULATIONS

Material Designation	Туре	Manufacturer
Sulfur	Vulcanizing agent for rubber	E. I. Du Pont De Nemours & Co., Inc. Wilmington 98, Delaware
Synvar RC-50-D	Thermosetting phenolic resin	Synvar Corp. Wilmington, Delaware
Tuads	Accelerator for vulcanizing rubber	Vanderbilt Co., Inc. 230 Park Ave. New York 17, New York
Trimene Base	Catalyst for cure of polyacrylic rubber	Naugatuck Chemical Co. 1230 Ave. of the Americas New York 20, New York
Varcum 5138	Thermoplastic resin	Varcum Chemical Corp. Niagara Falls, New York
Zinc Oxide	Vulcanizing agent for rubber	American Firstoline Corp. 420 Lexington Ave. New York 17, New York